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FINAL REPORT - EFFECT OF LUBRICATION OF LAP JOINTS	THE JOINT BEARD	NG STRENGTH OF RIVETED				
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FRANKLIN, T. PERRY						
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	NAVAL AIR SYSTEMS COMMAND DEPARTMENT OF THE NAVY					

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DEPARTMENT OF THE NAVY

NAVAL AIR DEVELOPMENT CENTER WARMINSTER, PA. 18974

AIR VEHICLE TECHNOLOGY DEPARTMENT

REPORT NO. NADC-72055-VT

4 APRIL 1972

EFFECT OF LUBRICATION ON THE JOINT BEARING STRENGTH OF RIVETED LAP JOINTS

FINAL REPORT
AIRTASK NO. A05-530/202-1/2000000000
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This report contains the results of an investigation of joint shear strengths using solid rivet fasteners lubricated with lauric acid.

Reported by Frondlin J. Jean

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Aero Materiala

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EVALUATION AND DISCUSSION

INTRODUCTION

The yield and ultimate shear strength of joints fabricated from various metals using solid river fasteners lubricated with lauric acid is reported herein. The results of the investigations showing a reduction of material bearing strength when pins and threaded fasteners were lubricated with lauric acid have been reported in references (a) and (b) respectively.

TEST PROCEDURE

Joint yield and ultimate strengths were determined in accordance with reference (c), using a Tinius Olsen Universal Testing Machine, Model Super "L" UTM Serial 54984-3, and a Baldwin Extensometer, Model TSMD Serial 1029 (Figures 1 and 2). All the rivets and sheet material were initially cleaned ultrasonically in chlorothene V.G.S.A. 1192A. Tests were performed on the clean riveted lap joint specimens, and the yield and ultimate strength was recorded. To determine the effect of lubrication, rivets were then costed with lauric acid (CH₃(CH₂)₁₀COOH) and specimens fabricated. The tests were repeated. The test specimens were .063 inches thick, and the rivet holes in the specimens were within a tolerance range of .253 to .257 inches. The installation requirements to form the flat driven heads on the rivets used in the test were in accordance with reference (d).

The four materials used in this investigation included aluminum (2024-T3 Sheet-Heats 1-2), magnesium (AZ31B-H24 Sheet), and steel (PHi5-7 Mo Sheet). Rivets of the following types and the driving pressures that were required to form the fastener heads in the lap joints are shown below:

Type	Material	Driving Pressure
MS 20470D8-6	Aluminum	12,000 lbs.
NS 20470B8-6	Magnesium	9,000 lbs.
NAS 1198-8-6	Steel	22,000 lba.

DISCUSSION

All specimens were subjected to the joint shear test specified in reference (c). One half of the ultrasonically cleaned specimens were tested with rivets that had been lubricated with lauric acid. Careful control of all significant parameters was exercised to determine any effect upon the lap joints' bearing yield and bearing ultimate strength produced by lubrication of the rivets.

Joint yield strength was determined from load deflection curves using the second modulus method for hole filling fasteners in accordance with reference (c). The bearing yield loads are shown on the load deflection charts, Figures 3 through 82. The joint bearing yield and bearing ultimate strength was calculated by dividing the applicable load carried by the bearing area. The results obtained are shown in Tables I through VIII. The average strength of the lap joint specimens tested with lubricated rivets was consistently lower than those of the specimens tested with non-lubricated rivets, Table IX.

CONCLUSIONS

It is concluded that joints fabricated with lubricated rivets, like those fabricated with lubricated threaded fasteners, have lower bearing yield and bearing ultimate joint strengths than when fabricated with clean fasteners.

RECOMMENDATIONS

It is recommended that this effect be considered in the preparation of MIL-HDBK-3 since the reductions are not the same for hole filling fasteners (rivets), non-hole filling fasteners (bolts), and sheet materials.

REFERENCES

- (a) NAVAIRDEVCEN Report No. NADC-MA-7007 of 31 Dec 1970, Effect of Lubrication on the Bearing Strength of Various Metallic Materials
- (b) NAVAIRDEVCEN Report No. NADC-MA-7162 of 27 Sep 1971, Effect of Lubrication on the Joint Bearing Strength of Metal Joints
- (c) MIL-STD-1312 Notice 1 Test 4, Joint Shear Strength
- (d) NAVAIR 01-1A-8 Technical Manual Structural Hardware

ALUMINUM 2024-T3 HEAT-1 (ALCOA)

	NOT LUBRICATI	S.D.	LUBETCATEL					
SPECIMEN NO.	BEARING VIELD STRENGTH (PSI)	BEARING ULTIMATE STHEROIT (PSI)	SPECIMEN NO.	BEARING VIELS STRENGTH (P. 1)	BEARING LETIMATE			
l-A	101,269	138,095	4-AW	93,650	106,031			
2-A	101,587	135,238	3-AW	91,746	111,111			
3 - A	101,587	136,507	5-AW	91,746	114,920			
5 - A	101,904	136,825	2-AW	92,063	116,825			
7 - A	98,412	136,825	6-AW	90,793	118,095			
AVG.	100,951	136,698		91,999	113,346			

NOTE:

- 8.8% decrease in bearing yield strength when lubricated.
- 17.0% decrease in bearing ultimate strength when lubricated.

ALUMINUM 2024-T3 HEAT-2 (HARVEY)

	NOT LUBRICATI	ED	LUBRICATED						
SPECIMEN NO.	SEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)				
2∾н	103,174	136,507	12-HW	90,476	111,746				
3 - H	107,396	137,142	14~HW	89,841	113,333				
4 - H	108,888	137,777	18-HW	90,158	115,555				
7 - H	106,349	139,047	11-HW	87,619	117,460				
1-H	99,682	145,396	16-HW	93,333	119,682				
AVG.	105,097	139,173		90,285	115,555				

NOTE:

14.0% decrease in bearing yield strength when lubricated.

16.9% decrease in bearing ultimate strength when lubricated.

Magnes Ium H-5070 (DOW)

	NOT LUBRICATE	I.	LUBRICATED					
SPECIMEN NO.	BEARING VIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YJELD STRENGTH (PSI)	EEARING ULTIMATE STRENGTH (PSI)			
3-D	66,349	86,349	15-DL	60,317	83,809			
1-D	71,428	88, 571	18-DL	63,492	83,492			
6-D	72,065	88,888	17-DL	60,372	84,444			
7 - D	65,714	89,523	10-DL	66,031	87,301			
11-D	65,079	90,476	16-DL	61,904	86,031			
AVG.	68,126	88,761		62,423	85,015			

NOTE:

- 8.3% decrease in bearing yield strength when lubricated.
- 4.2% decrease in bearing ultimate strength when lubricated.

MAGNESIUM 7546 AZ31B

***************************************	NCT LUBRICAT	ED		LUBRICATED	
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
2-M	67,619	82,539	, 4-ML	58,412	79,047
5 -M	68,571	85,079	. I-ML	58,095	81,904
3-M	68,253	85,714	8-MI,	57,142	81,904
4-M	68,888	86,984	6-ML	60,317	81,904
10-M	69,841	: 88,253 [']	5 -ML	59,365	82,539
AVG.	68,634	85,713		58,666	81,459
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NOTE:

14.5% decrease in bearing yield strength when lubricated.

4.9% decrease in bearing ultimate strength when lubricated.

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MAGNESIUM : C-70065 (DOW)

	NOT LUBRICATE	D'	LUBRICATED					
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN 1	BEARING YIELD STRENGTH (PSI)	PEARING ULTIMATE STRENGTH (PSI)			
D-`2	60,317	82,222	13-DL	55,555	77,142			
p÷1	60,317	82,857	16-DL	55,873	78,412			
D-5	60,634	83,492	10-DL	55,873	78,730			
D=7	63,492	84,126	12-DL	57,142	79,882			
D-8 ;	60,634	85,398	11-DL	56,825	80,000			
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AVG.	61,078	83,619		56,253	78,833			
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NOTE:

- 7.8% decrease in bearing yield strength when lubricated.
- 5.7% decrease in bearing ultimate strength when lubricated.

NADC-72055-VT

STEEL 870255

	NOT LUBRICAT	ED	LUBRICATED					
SPECIMEN NO.	BEARING YIELD STRENGTH (FSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)			
SA-4	126,666	229,841	SAL-8	104,761	205,714			
SA-9	133,650	234,920	SAL-1	104,761	204,444			
SA-2	133,333	228,571	SAL-4	93,650	195,873			
SA-5	126,984	228,253	SAL-6	101,587	182,539			
SA-6	139,682	225,079	SAL÷9	107,936	208,888			
AVG.	132,063	229,332		102,539	199,491			

NOTE:

22.3% decrease in bearing yield strength when lubricated.

13.0% decrease in bearing ultimate strength when lubricated.

STEEL 851064

	NOT LUBRICATE	D		LUBRICATED	
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
SB-3	101,587	208,571	SBL-9	111,111	193,650
SB-5	120,634	213,650	SBL-3	117,460	196,190
SB-4	129,841	214,920	SBL-7	104,761	199,365
SB-2	123,809	215,555	SBL-4	111,111	187,619
SB-7	128,571	215,873	SBL-5	117,460	187,619
AVG.	120,888	213,713		112,380	192,888

NOTE:

- 7.0% decrease in bearing yield strength when lubricated.
- 9.7% decrease in bearing ultimate strength when lubricated.

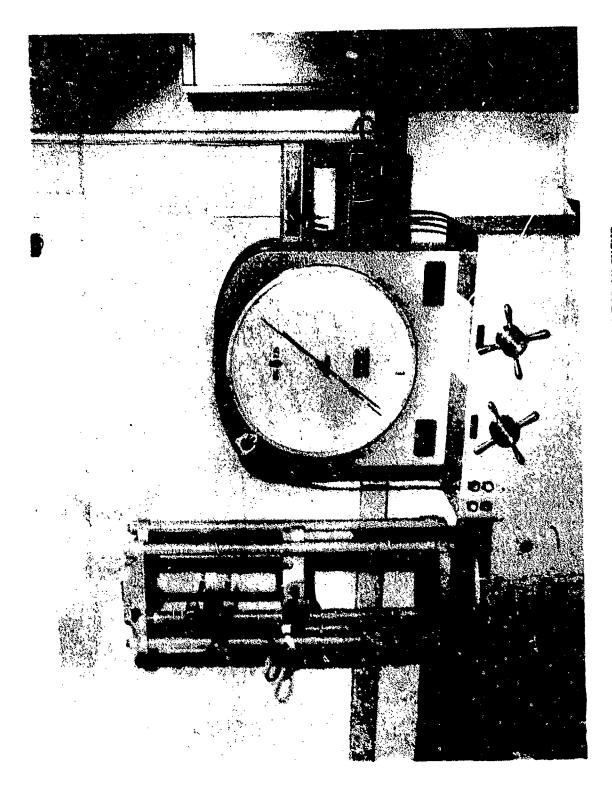
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STEEL 861104

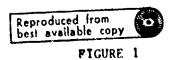
	NOT LUBRICAT	ED		LUBRICATED	
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
SC=6	117,460	215,555	SCL-18	114,285	196,190
sc-4	123,174	216,507	SCL-12	104,761	193,015
SC-7	120,634	219,047	SCL-15	107,936	191,111
SC=3	125,396	219,047	SCL-17	111,111	186,349
\$ C+ 5	128,23 5	226,349	SCL-11	111,111	205,079
AVG.	123,047	219,301		109,840	194,348

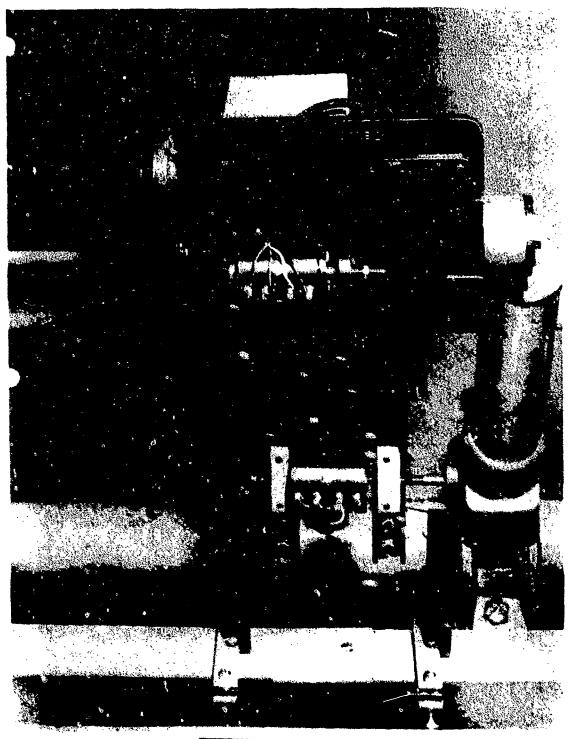
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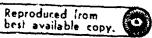
- 10.7% decrease in bearing yield strength when lubricated.
- 11.3% decrease in bearing ultimate strength when lubricated.



TINIUS OLSEN 60,000 LB. UNIVERSAL TESTING MACHINE

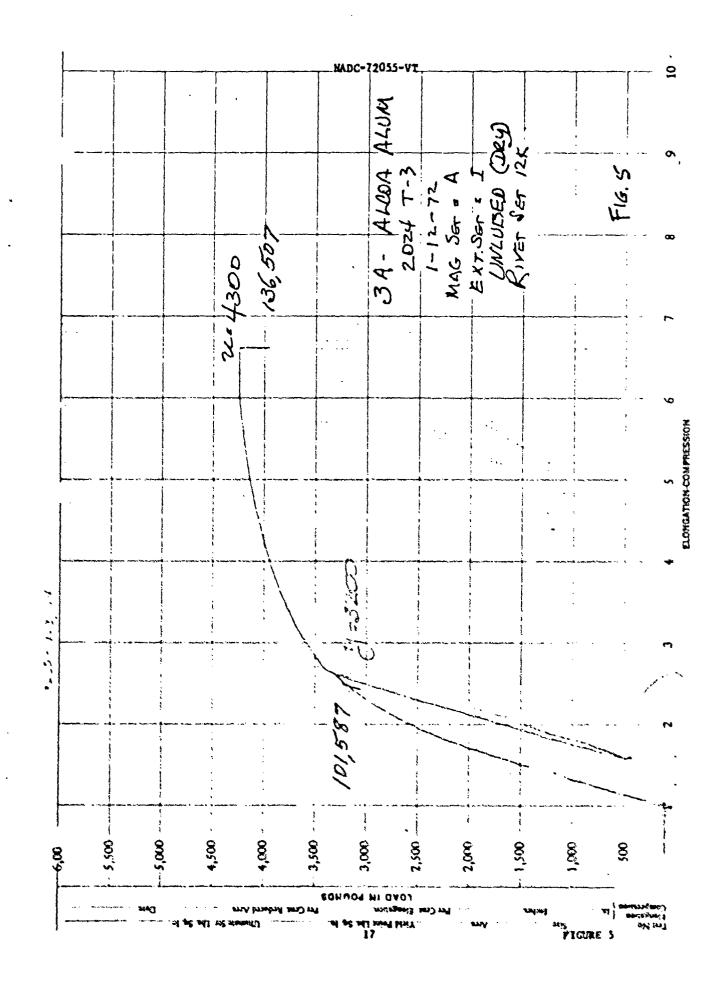






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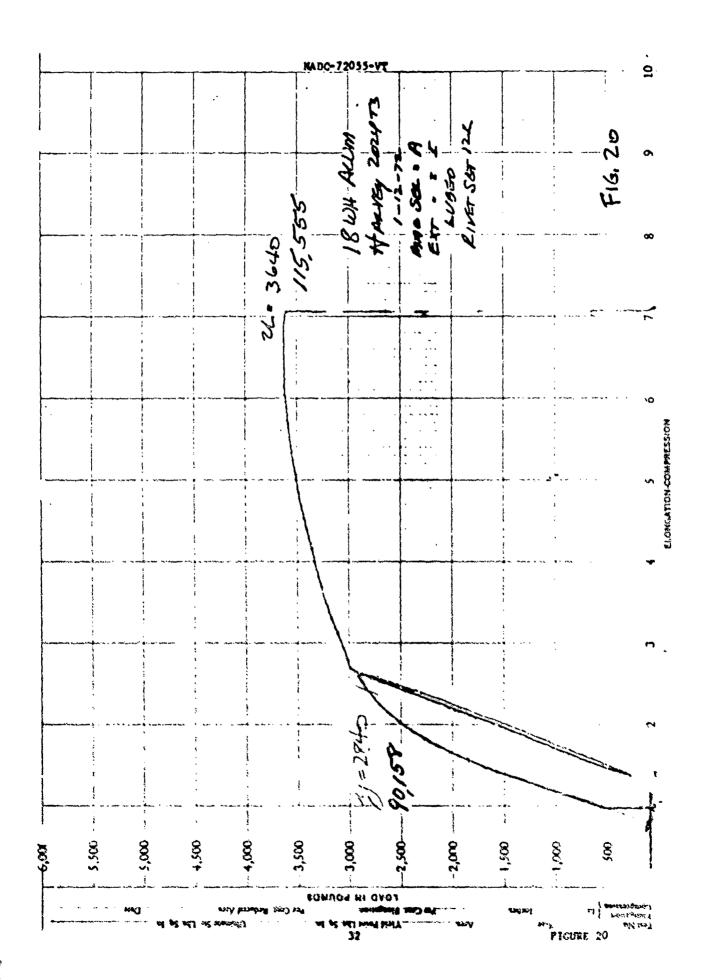
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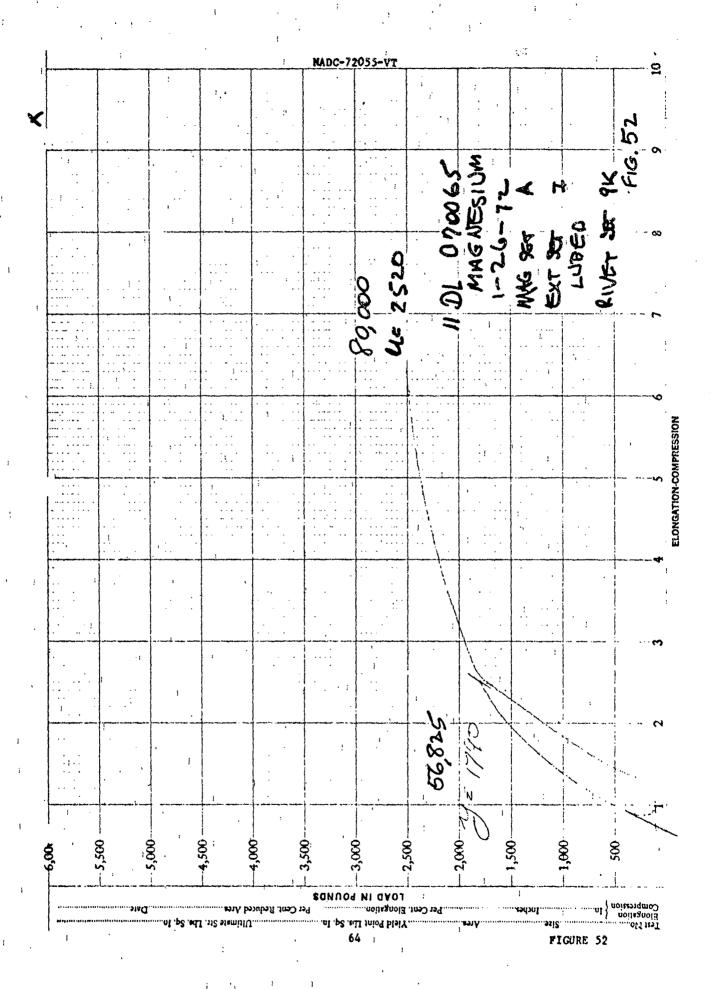
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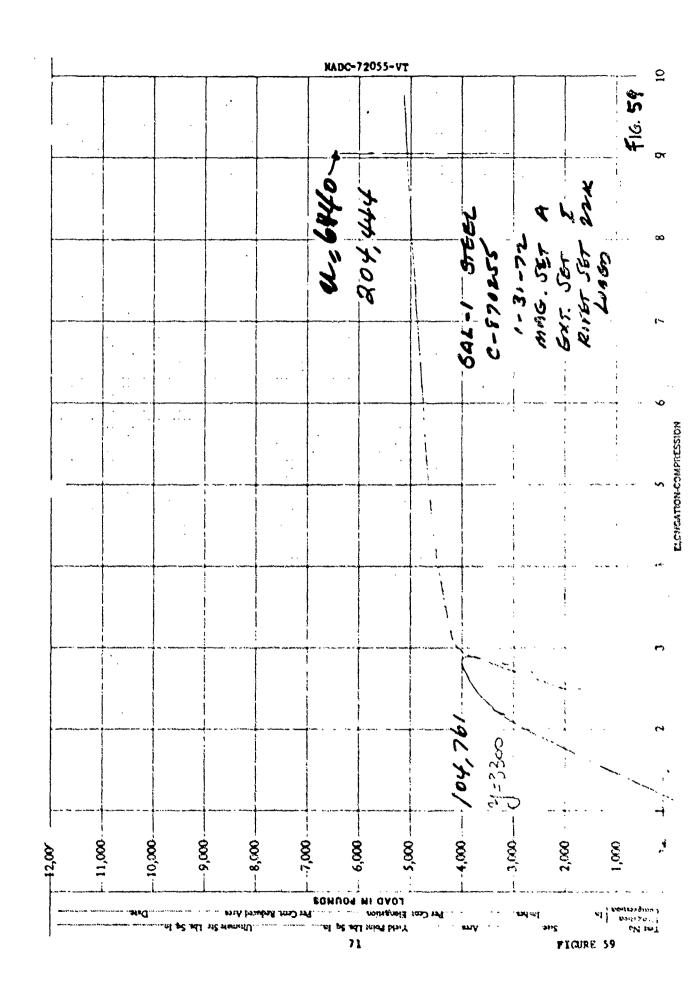
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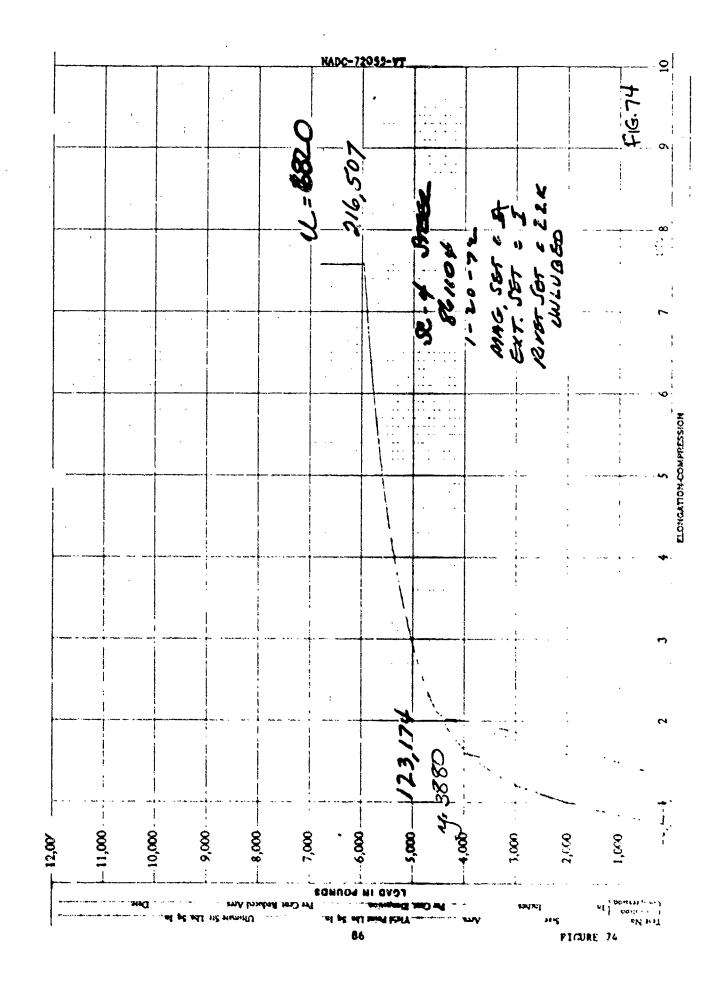
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